

LONG TERM STUDIES ON COMPRESSIVE STRENGTH OF HIGH VOLUME NANO PALM OIL FUEL ASH MORTAR MIXES

Mohd Warid Hussin^a, Nor Hasanah Abdul Shukor Lim^{b*}, Abdul Rahman Mohd. Sam^c, Mostafa Samadi^b, Mohamed A. Ismail^d, Nur Farhayu Ariffin^b, Nur Hafizah A. Khalid^b, Muhd Zaimi Abd Majid^a, Jahangir Mirza^a, Habeeb Lateef^b

Article history

Received
2 July 2015
Received in revised form
20 October 2015
Accepted
23 October 2015

*Corresponding author
amoi_1464@yahoo.com

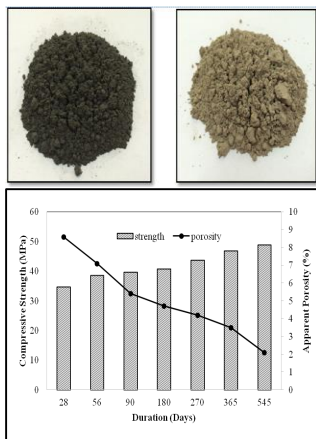
^aUTM Construction Research Centre, Institute for Smart Infrastructure and Innovative Construction, Faculty of Civil Engineering, Universiti Teknologi Malaysia, 81310 UTM Johor Bahru, Johor, Malaysia

^bConstruction Material Research Group (CMRG), Department of Structures and Materials, Faculty of Civil Engineering, Universiti Teknologi Malaysia, 81310 UTM Johor Bahru, Johor, Malaysia

^cDepartment of Structures and Materials, Faculty of Civil Engineering, Universiti Teknologi Malaysia, 81310 UTM Johor Bahru, Johor, Malaysia

^dDepartment of Architectural Engineering, Hanyang University, Ansan, Republic of Korea

Graphical abstract



Abstract

Palm oil fuel ash is a waste material that can be used as partial cement replacement. However, its reactivity as pozzolanic material depends on the size of the particle. This paper presents the effects of nano size palm oil fuel ash on the long term characteristics of mortar. The study covers basic properties of mortar including the morphology, porosity, compressive strength and microstructural with regards to the variations in the mix design of the mortar. The palm oil fuel ash used has gone through heat treatment and was ground to a nano size with the percentage replacement of cement used was 60%, 80% and 100%. The different types of mortar samples were cast in a 70x70x70mm cube for compressive strength test. All casting and testing of the samples were conducted in the laboratory at ambient temperature. The results show that the use of 80% nano size palm oil fuel ash has produced higher compressive strength at the age of 28 days by 32% compared to the control mortar. Grinding the palm oil fuel ash to a nano size particle has improved the reactivity of the ash and because of it is a waste material it reduces the cost of the mortar. The experimental result also show that the compressive strength of the 80% nano size palm oil fuel ash mortar at 365 days was 25% higher than its strength at 28 days. In addition, the porosity of the 80% nano palm oil fuel ash mortar was reduced by 51% at the age of 1 year. The overall results have revealed that the use of high volume nano palm oil fuel ash can enhance the mortar properties and due to the high percentage of replacement it can contribute to a more sustainable construction.

Keywords: Palm oil fuel ash, nano size, high volume, porosity, strength development

© 2015 Penerbit UTM Press. All rights reserved

1.0 INTRODUCTION

Huge amount of carbon dioxide is emitted into the atmosphere during cement manufacturing. Around 7% of the total carbon dioxide all over the world come from cement manufacturing according to the Intergovernmental Panel on Climate Change (IPCC) report in 2005 [1]. From 2005 to 2030 world cement manufacturing will increase yearly which could cause the level of carbon emission to reach 1.7 times more than what it was in 2005 [2, 3]. This carbon emission has negative effect on environment that causes global warming which concerns many researchers [4-6].

The need towards sustainability and sustainable environment has made the use of pozzolanic material in mortar popular. Therefore, reusing the abundant waste materials has become necessary especially wastes produced from palm oil manufacturing. One of the latest additions of pozzolanic material is palm oil fuel ash (POFA) [7-9]. POFA is a by-product from biomass thermal power plants where oil palm residues are burned to generate electricity [10] (Figure 1.)

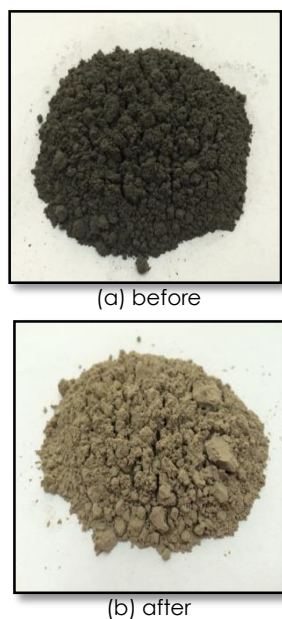


Figure 1 POFA colour before and after heat treatment

Few studies have been done by other researchers on the replacement of partial weight of cement by POFA [11, 12], but there still remains high amount of ash abundantly available in the landfill which lead to environmental problems. It is reported that the maximum strength gain occurred at the cement replacement level of 30% POFA with the size of 45 μm . Further increment in the ash content would reduce the strength of mortar gradually [9].

Tangchirapat and Jaturapitakkul [13] reported that increasing the fineness of POFA has positive effect on the reduction of drying shrinkage and permeability of

concrete. However none of researchers have studied the effect of POFA in nano size. The short term performances of nano palm oil fuel ash have been studied as cementitious materials in terms of chemical and physical properties [14, 16].

Therefore, in this paper, the long term effects of high volume of POFA with nano size used as cement replacement up to 80% were investigated. This could help prolong the age of mortar besides reducing the usage of expensive nano admixture for increasing compressive strength of mortar and carbon dioxide gas emission from cement production process.

2.0 EXPERIMENTAL

2.1 Materials

The cement used in this study complies with Portland cement Type I as stated in the ASTM C 150-12 [16]. POFA was obtained from the burning of palm oil shell and husk (in equal volume) at 450°C from a palm oil mill in Johor Malaysia. The collected ashes were dark in colour as shown in Figure 1 and the loss on ignition (LOI) was 20.9% for ground POFA. POFA has low pozzolanic reactivity due to its large particle size and porous structure [17]. Therefore, POFA has been treated and ground until nano size to increase the pozzolanic reactivity and to remove the unburned materials. Details of POFA treatment and its chemical compositions are presented in other published work [14, 15].

In the preparation process for all specimens, the fine aggregates (sand) were used in the saturated surface dry condition to reduce water absorption during mixing process [18, 19]. Fine aggregates were sieved through 2.35 mm sieve and retained at 300 μm before storing in the airtight container. Figure 2 shows the sieve analysis test on the fine aggregates. The grading curve for fine aggregates was within the limit line prescribed according to ASTM C33-03[20].

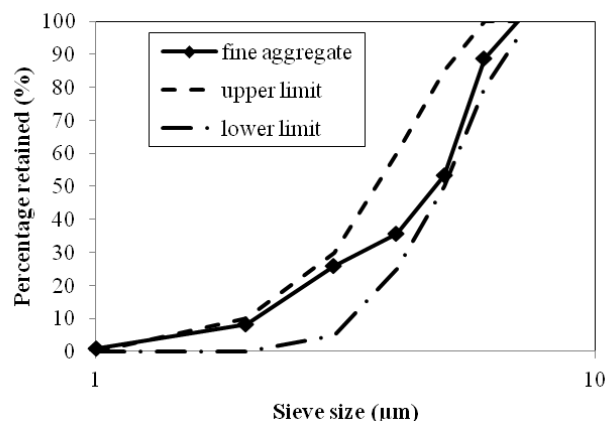


Figure 2 Sieve analysis for sand

2.2 Testing Procedures

All mortar specimens were prepared with sand to binder ratio of 3:1, whereby the sand was prepared into saturated surface dry condition. The mixing was carried out in a room temperature. The mix proportions are given in Table 1 based on weight of materials according to BS EN 998-1:2010 [21]. 60%, 80% and 100% of POFA were used as cement replacement. The test specimens of 70 x 70 x 70 mm cubes were prepared. The specimens were compacted in two-layers with rod tamping as described in ASTM C109-13 [22]. Additional vibration of about 10s was applied using the vibrating table. The test specimens were cured in water for 7, 14 and 28 days.

The particle size of POFA was measured using transmission electron microscopy (TEM). The morphology of POFA mortar was investigated by using field emission scanning electron microscopy (FESEM). The surface of the specimens obtained from the compressive strength test was coated with gold prior to their morphological observation.

Determination of apparent porosity of mortars was done according to ASTM C1403-13 [23]. Three cubes of mortars were oven-dried at 85°C for 24 hours and then immersed in water for 48 hours. The cubes were further suspended in water and weighted. The data were recorded and calculated for average.

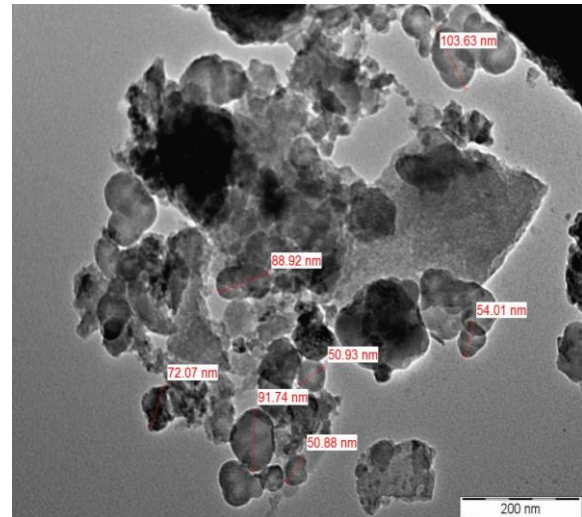


Figure 3 TEM test result for nano POFA

3.2 Compressive Strength

Figure 4 shows the strength development of OPC, 60%, 80% and 100% POFA mortar for more than one year. All the mortar mixes showed increment in compressive strength with the increasing duration of water curing. OPC mortar showed gradual increasing after 28 days meanwhile the specimens with 60% and 80% POFA mortar produced very high compressive strength at age of 28 days. This is due to the pozzolanic reaction between excessive Ca(OH)_2 formed from hydration process of cement with silica (SiO_2) of POFA. These, produce more C-S-H gel and make the mortar denser and more durable. Again, this showed that the packing effect of small particle size and pozzolanic reaction was fully involved [24]. However, the specimens with 100% POFA provided very low strength even at later age which was about 5 MPa. This is due to the lack of CaO content to produce Ca(OH)_2 for pozzolanic reaction to take place.

Table 1 Mix proportion of mortar

Materials	Mortar mix			
	OPC	60% POFA	80% POFA	100% POFA
Cement (kg/m ³)	525	210	105	-
POFA (kg/m ³)	-	315	420	525
Sand (kg/m ³)	1578	1578	1578	1578
w/c ratio	0.4	0.4	0.4	0.4

3.0 RESULTS AND DISCUSSION

3.1 Determination of Particle Size of POFA

The particle size of POFA was examined using transmission electron microscopy (TEM) technique. As shown in Figure 3, the particle size of POFA varied between 50-100 nm. The figure shows that POFA has spherical, crushed and irregular shape [14, 15].

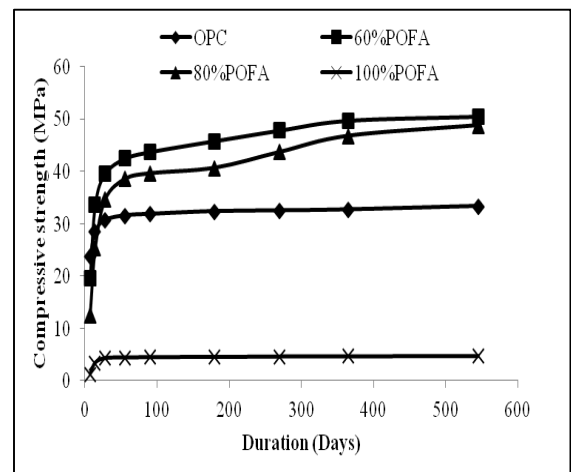


Figure 4 Strength development of POFA mortar up to 1.5 years

3.3 Porosity

Figure 5 shows the test results for apparent porosity of mortar mixes for more than one year. The results clearly indicated that the use of nano POFA reduced the porosity of mortar mixes at all ages. At early ages, the recorded porosity for high volume POFA mortar was higher compared with OPC mortar. This is due to the incomplete reaction between the binders. In addition, by increasing the POFA content from 60% to 100%, the porosity increases from 7.5% to 10%. However, the porosity for all POFA mortar reduces with the longer period of water curing. This is due to the hydration process and pozzolanic reaction during the period which was responsible for the reduction in porosity and the increase in strength of mortar.

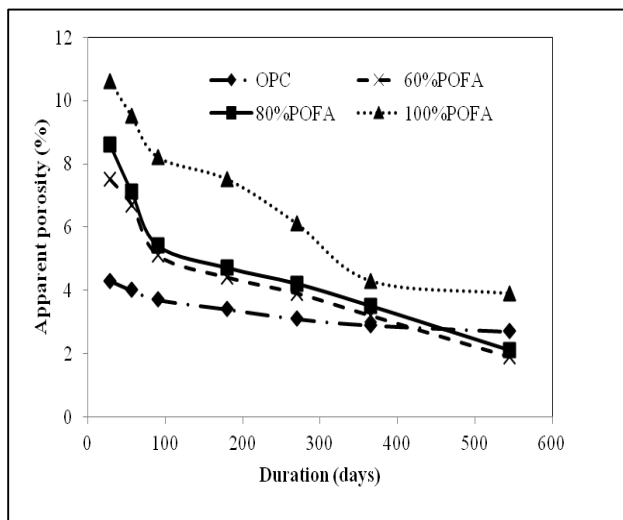


Figure 5 Apparent porosity of mortar mixes

3.4 Strength Development vs Porosity

Porosity of the mortars highly influences the strength of mortar. The reduction of porosity in mortar will increase its strength and makes it dense. Figure 6 shows the result of strength development and apparent porosity of 80% POFA replacement in water curing for more than one year. As shown in Figure 6, the 28 days apparent porosity was recorded as 8.6 % while the strength was 35 MPa. Prolonged curing period has shown to lower the porosity and increase the strength of the mortar. After 365 days of curing, the porosity was 3.5 % and the compressive strength was 47 MPa. The porosity decreased at 365 days which was recorded almost 51 % lower than its initial porosity. In the meantime, the compressive strength increased by 25 % from initial strength. This is due to the complete reaction between Ca(OH)_2 and SiO_2 from POFA that produced more C-S-H gel. Besides, the extra POFA also reacted as filler thus help reduce the porosity of mortar. Porosity has a significant effect on compressive strength of mortar [25].

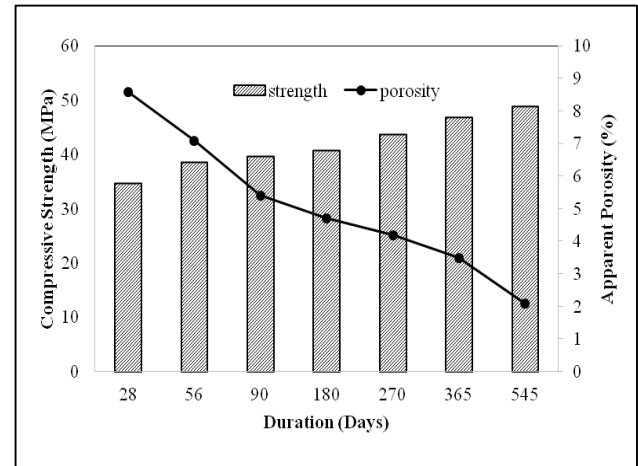


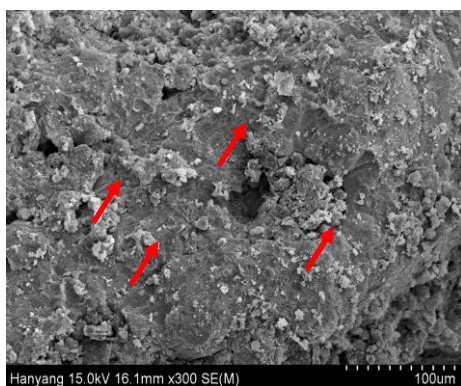
Figure 6 Relationship between compressive strength and porosity of 80% POFA replacement

3.5 Morphology of POFA Mortar

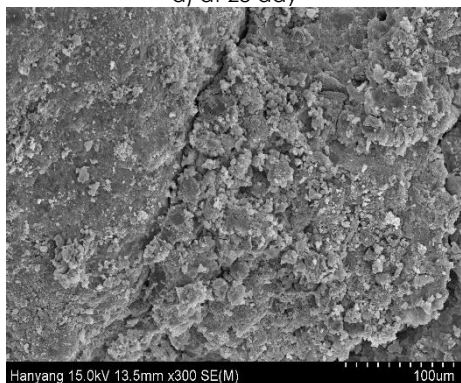
The microstructure of mortar was studied using Field Emission Scanning Electron Micrograph (FESEM) techniques. The porosity of mortar can be observed by using the FESEM techniques [26]. By increasing the age of curing the sample contains 80% POFA as cement replacement, the total amount of calcium silicate hydrated (C-S-H) crystals increased which consequently reduced the porosity. As shown in Figure 7, the specimens at 365 days carry fewer voids compared with specimens at 28 days. The ability of pozzolanic material to reduce the amount of Ca(OH)_2 in the paste has also been proved by previous researchers [27].

4.0 CONCLUSIONS

Based on the test results obtained it can be concluded that nano size POFA enhanced the properties of mortar and can be used up to 80% replacement of cement. The compressive strength of mortar with 80% POFA showed better strength at later age due to the pozzolanic reaction. The porosity recorded for POFA specimens decreased to almost 51% while the compressive strength increased by 25% from initial strength.



a) at 28 day



b) at 365 days

Figure 7 FESEM image of 80% POFA mortar at different ages

Acknowledgement

The authors are grateful to the Ministry of Higher Education, Malaysia (MOHE) and Research Management Centre (RMC), Universiti Teknologi Malaysia (UTM) for the financial support under grant GUP Q.J130000.2509.06H56 and grant GUP Q.J130000.2517.07H32. The authors are also thankful to the staff of Structures and Materials Laboratory, Faculty of Civil Engineering for their support throughout the study.

References

- [1] Metz, B., Davidson, O. R., Bosch, P. R., Dave, R. and Meyer, L. A. 2007. *Climate Change 2007. Contribution Of Working Group III To The Fourth Assessment Report Of The Intergovernmental Panel On Climate Change*. Cambridge, United Kingdom and New York, NY, USA: University Press.
- [2] Akashi, O., Hanaoka, T., Matsuoka, Y. and Kainuma, M. 2011. A Projection For Global CO₂ Emissions From The Industrial Sector Through 2030 Based On Activity Level And Technology Changes. *Energy*. 36(4): 1855-1867.
- [3] Asipita, Salawu Abdulrahman, Mohammad Ismail, Muhd Zaimi Abd Majid, Zaiton Abdul Majid, Che Sobry Abdullah, and Jahangir Mirza. 2014. Green Bambusa Arundinacea Leaves Extract As A Sustainable Corrosion Inhibitor In Steel Reinforced Concrete. *Journal of Cleaner Production*. 67: 139-146.
- [4] Nasiru Zakari Muhammad, Ali Keyvanfar, Muhd Zaimi Abd Majid, Arezou Shafaghat, Jahangir Mirza. 2015.

- Waterproof Performance Of Concrete: A Critical Review On Implemented Approaches. *Construction and Building Materials*. 101P1(2015): 80-90 (DOI: 10.1016/j.conbuildmat.2015.10.048).
- [5] Talaiekhazani, A., Keyvanfar, A., Andalib, R., Samadi, A., Shafaghat, A., Kamyab, H., Majid, M. Z., Zin, R. M., Fulazzaky, M. A., Lee, C. T., and Hussin, M. W. 2014. Application of Proteus Mirabilis And Proteus Vulgaris Mixture To Design Self-Healing Concrete. *Desalination and Water Treatment*. 52: 19-21, 3623-3630.
 - [6] Mohamad, M. E., I. S. Ibrahim, R. Abdullah, AB Abd Rahman, A. B. H. Kueh, and J. Usman. 2015. Friction and Cohesion Coefficients Of Composite Concrete-To-Concrete Bond. *Cement and Concrete Composites*. 56(1-14).
 - [7] Hussin, M. W. and Abdul Awal. 1996. Influence of Palm Oil Fuel Ash on Strength and Durability of Concrete. In: *Proceedings of the 7th International Conference on Durability of Building Materials and Components*, Stockholm, Sweden. 19-22 May. 1: 291-298.
 - [8] Awal, A. S. M. A. 1998. A study of Strength and Durability Performances of Concrete Containing Palm Oil Fuel Ash. Universiti Teknologi Malaysia. PhD Thesis.
 - [9] Sumadi, S. R. 1993. Relationships between Engineering Properties and Microstructural Characteristics of Mortar Containing Agricultural Ash. Universiti Teknologi Malaysia. PhD Thesis.
 - [10] Khalil, H. P. S. A., Fizree, H. M., Bhat, H., Jawaid, M. and Abdullah, C.K. 2013. Development and Characterization Of Epoxy Nanocomposites Based On Nano-Structured Oil Palm Ash. *Comp Part B: Engineering*. 53: 324-333.
 - [11] Awal, A. S. M. A. and Abubakar, S. I. 2011. Properties of Concrete Containing High Volume Palm Oil. *Malaysian J. Civil Eng.* 23(2): 54-66.
 - [12] Taha, M., Mohammad, I., Salihuddin, R. S., Bhutta, M. A. R., Mostafa, S. and Seyed, M. S. 2014. Binary Effect Of Fly Ash And Palm Oil Fuel Ash On Heat Of Hydration Aerated Concrete. *The Scientific World Journal*. 46: 12-41.
 - [13] Tangchirapat, W. and Jaturapitakkul, C. 2010. Strength, Drying Shrinkage, And Water Permeability Of Concrete Incorporating Ground Palm Oil Fuel Ash. *Cem Concr Compos.* 32(10): 767-774.
 - [14] Hasanah, N. S. A., Hussin, M. W., Sam, A. R. M., Bhutta, M. A. R. and Samadi, M. 2015. Properties of Mortar Containing High Volume Palm Oil Biomass Waste. *Advanced Materials Research*. 1113: 578-585.
 - [15] Lim, N. H. A. S., Ismail, M. A., Lee, H. S., Hussin, M. W., Sam, A. R. M., and Samadi, M. 2015. The Effects Of High Volume Nano Palm Oil Fuel Ash On Microstructure Properties And Hydration Temperature Of Mortar. *Construction and Building Materials*. 93: 29-34.
 - [16] ASTM C 150. 2012. Standard Specification For Portland Cement. West Conshohocken: ASTM International: 2012.
 - [17] Anderson, J. E., Meryman, H. and Porsche, K. 2007. Sustainable Building Materials in French Polynesia. *International Journal for Service Learning in Engineering*. 2: 102-130.
 - [18] Ariffin, N. F., Hussin, M. W., Rahman, A. S. M., Bhutta, M. A. R., Hasanah, A. S. L. and Hafizah, A. K. 2015. Degree of Hardening of Epoxy-Modified Mortars without Hardener in Tropical Climate Curing Regime. *Advanced Materials Research*. 1113: 28-35.
 - [19] Bhutta, M. A. R., Hasanah, N., Farhayu, N., Hussin, M. W., Tahir, M. B. M., and Mirza, J. 2013. Properties Of Porous Concrete From Waste Crushed Concrete (Recycled Aggregate). *Construction and Building Materials*. 47: 1243-1248.
 - [20] ASTM C33. 2003. Standard Specification for Concrete Aggregates. West Conshohocken: ASTM International: 2003.
 - [21] British Standards Institution. 2010. Specification for Mortar For Masonry. Rendering And Plastering Mortar. BS EN 998-1: 2010.

- [22] ASTM C109. 2013. Standard Test Method for Compressive Strength of Hydraulic Cement Mortars (Using 2-in. or [50-mm] Cube Specimens). West Conshohocken: ASTM International: 2013.
- [23] ASTM C1403-14. 2014. Standard Test Method for Rate of Water Absorption of Masonry Mortar.
- [24] Awal, A. S. M. A. and Shehu, I. A. 2013. Evaluation of Heat Of Hydration Of Concrete Containing High Volume Palm Oil Fuel Ash. *Fuel Journal*. 105: 728-731.
- [25] Noruzman, A. H., Bala, M., Mohammad, I. and Majid, Z. A. 2012. Characteristics of Treated Effluents And Their Potential Applications For Producing Concrete. *Journal Of Environmental Management*. 110: 27-32.
- [26] Mirza, J., Saleh, K., Langevin, M. A., Mirza, S., Bhutta, M. A. R., and Tahir, M. M. 2013. Properties of Microfine Cement Grouts At 4°C, 10°C And 20°C. *Construction and Building Materials*. 47: 1145-1153.
- [27] Marianne, T. J., Dorte, M., Christian M. P. and Dirch, B. 2001. Durability of Resource Saving Green Type Of Concrete. In: *Proceedings Of FIB - Symposium On Concrete And Environment, Berlin, October*.